

## Specification

### Title of the Invention

5           A Complex Lens for a Tandem Scanning Optical System and a  
Manufacturing Method thereof

### Background of the Invention

10           The present invention relates to a complex lens that  
consists of a plurality of stacked lens portions, and  
particularly, relates to the complex lens for a tandem scanning  
optical system employed in an imaging device such as a color  
laser printer for converging a plurality of light beams  
15           deflected by a deflector. Further, the present invention  
relates to a manufacturing method of such a complex lens for a  
tandem scanning optical system.

          A tandem scanning optical system employed in a color laser  
printer is provided with four semiconductor lasers and four  
20           photoconductive drums that correspond to colors Y (Yellow), M  
(Magenta), C (Cyan) and K (black), respectively. In such a  
tandem scanning optical system, it is preferable to make at  
least one part of the optical system shareable among the colors  
to downsize the system. The polygon mirror may be shared.

25           When a polygon mirror is shared, four light beams are

incident on the polygon mirror such that they are arranged in an auxiliary scanning direction, which is coincident with a direction of the rotation axis of the polygon mirror. The four light beams deflected by the polygon mirror are converged by an 5  $f\theta$  lens and the optical paths thereof are separated by mirrors. The separated four light beams form scanning lines on the respective photoconductive drums.

It is preferable that the four light beams deflected by the polygon mirror are converged by the respective lens 10 elements in order to obtain the most suitable optical performance. On the other hand, the smaller the thickness of the polygon mirror is, the smaller the spaces among the four light beams are in the vicinity of the polygon mirror. This does not allow employing independent lens elements for the 15 respective light beams. Therefore, a lens in the  $f\theta$  lens arranged close to the polygon mirror should be a complex lens that consists of stacked four lens portions.

#### Summary of the Invention

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It is therefore an object of the invention to provide an improved manufacturing method of a complex lens for a tandem scanning optical system that is capable of reducing the positional error among the lens portions when the complex lens 25 that consists of stacked lens portions is molded as a single-

piece element.

*Sub B* For the above object, according to the present invention, there is provided a manufacturing method of a complex lens for a tandem scanning optical system, including a step for 5 preparing molding dies for forming a cavity to form the complex lens as a single-piece element, and a step for injecting lens material into the cavity. The molding dies include a pair of single-piece mirror surface cores that form a plurality of lens surfaces of the complex lens at an incident side and a 10 plurality of lens surfaces at an exit side, respectively. The complex lens consists of a plurality of stacked lens portions for converging a plurality of light beams, which are modulated independently and deflected by a deflector, onto a surface to be scanned, respectively, for forming a plurality of scanning 15 lines at the same time.

Further, a complex lens for a tandem scanning optical system according to the present invention is formed as a single-piece element that is equivalent to a combination of independent lens portions stacked one on another, the lens 20 surfaces of the lens portions at the incident side are formed by a single-piece mirror surface core and the lens surface of the lens portions at the exit side are formed by another single-piece mirror surface core.

Since the lens surfaces at the incident side and the lens 25 surface at the exit side are formed by the single-piece mirror

surface cores, respectively, during the molding process, the relative positional error among the lens surfaces at the incident side and that at the exit side can be reduced.

It is preferable that each of the mirror surface portions 5 of the mirror surface cores has a concave sectional shape in a direction perpendicular to the direction in which a plurality of light beams scan (i.e., an auxiliary scanning direction). That is, the lens surfaces of the molded complex lens preferably have convex sectional shapes in the direction 10 perpendicular to the scanning direction of the light beam.

When the mirror surface portions of the mirror surface core have convex sectional shapes, the boundary of the mirror surface portions will be a valley. Therefore, the boundary portions cannot be sharply processed because of the limitation 15 of a cutting tool, which requires predetermined margins at the boundaries. The margins are not employed as lens surfaces.

On the other hand, when the mirror surface portions of the mirror surface core have concave sectional shapes, the boundary of the mirror surface portions will be a peak. Therefore, 20 since the boundary portions can be sharply processed by the cutting tool, the mirror surface portions can be processed without the margins.

The mirror surface portions of at least one of the mirror surface cores at the incident and exit sides may be formed as 25 rotationally-symmetrical concave surfaces with respect to

respective optical axes such as spherical surfaces. In such a case, the lens surfaces of at least one of the incident and exit sides are formed as rotationally-symmetrical convex surfaces with respect to respective optical axes.

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Brief Description of the Drawings

Fig. 1A is a sectional view of a cavity and surroundings of an injection molding machine to mold a complex lens for a tandem scanning optical system according to embodiments;

Fig. 1B is a sectional view of the complex lens molded by the injection molding machine of Fig. 1A;

Fig. 2 is a perspective view of a mirror surface core employed in the injection molding machine of Fig. 1A;

Fig. 3 is a sectional view of the injection molding machine to mold the complex lens of the embodiments;

Fig. 4 shows a tandem scanning optical system that employs the complex lens of Fig. 1B in the auxiliary scanning direction;

Fig. 5 shows a scanning optical system of a first embodiment in the main scanning direction;

Fig. 6 shows the scanning optical system of the first embodiment in the auxiliary scanning direction;

Fig. 7A is a graph showing a linearity error of the scanning optical system of the first embodiment;

Fig. 7B is a graph showing a curvature of field of the scanning optical system of the first embodiment;

Fig. 8 shows a scanning optical system of a second embodiment in the main scanning direction;

5 Fig. 9 shows the scanning optical system of the second embodiment in the auxiliary scanning direction;

Fig. 10A is a graph showing a linearity error of the scanning optical system of the second embodiment; and

10 Fig. 10B is a graph showing a curvature of field of the scanning optical system of the second embodiment.

#### Detailed Description of the Preferred Embodiments

A method for manufacturing a complex lens for a tandem scanning optical system will be described with reference to Figs. 1 through 3. Fig. 1A is a sectional view of a cavity and surroundings of an injection molding machine to mold the complex lens according to embodiments; Fig. 1B is a sectional view of the molded complex lens; Fig. 2 is a perspective view of a mirror surface core; and Fig. 3 is a sectional view of the injection molding machine.

The complex lens is formed as a single-piece element through an injection molding process. Molding dies used in the process include cores having mirror-finished surfaces to form 25 incident lens surfaces and exit lens surfaces of the lens

portions. The core is called a "mirror surface core" in this specification.

The general construction of the injection molding machine will be described with reference to Fig. 3. The machine is 5 provided with first and second retainer plates 2 and 3 that can slide in a right-left direction in the drawing in cylinders 1a and 1b located at right and left sides. The retainer plates 2 and 3 have hollows at the faces opposed to each other and mirror surface cores 4 and 5 are installed in the hollows, 10 respectively. A cavity 6 is formed as a space surrounded by molding dies, which include the first and second retainer plates 2, 3, and the mirror surface cores 4 and 5, when the retainer plates 2 and 3 close to contact with each other. Further, the first and second retainer plates 2 and 3 are 15 connected with driving rods 7 and 8, respectively, and the movement of the rods 7 and 8 in the right-left direction drives the retainer plates 2 and 3 to close them up and to move them away.

During the molding process, as shown in Fig. 3, the first 20 and second retainer plates 2 and 3 get closer to contact with each other and molten resin is injected into the cavity 6 through a runner (not shown). After the predetermined cooling time is elapsed from the injection, the retainer plates 2 and 3 are moved away and the molded complex lens is retrieved from 25 the molding dies.

The molded complex lens 20 is formed as a single-piece

element that is equivalent to a combination of independent four lens portions stacked one on another, as shown in Fig. 1B. The complex lens 20 has four incident lens surfaces 21 and four exit lens surfaces 22. In Fig. 1B, an x-direction is a  
5 direction parallel to each of optical axes of the lens portions, a y-direction is a direction along which the light beams are deflected by a polygon mirror (referred to as a main scanning direction), and a z-direction is a direction perpendicular to the x- and y-directions (referred to as an  
10 auxiliary scanning direction). The incident lens surfaces 21 and the exit lens surfaces 22 have convex sectional shapes in the auxiliary scanning direction. Further, in Fig. 1B, the convex shapes of the lens surfaces are exaggerated for purposes of illustration.

15 The incident lens surfaces 21 are formed (i.e., molded) by the single-piece mirror surface core 4 and the exit lens surfaces 22 are formed (i.e., molded) by the single-piece mirror surface core 5. As shown in Fig. 1A and Fig. 2, the mirror surface core 4 is formed as a single-piece element and  
20 is provided with four mirror surface portions 4a that are formed independently to form four lens surfaces. The mirror surface portions 4a have concave sectional shapes in both of the main and auxiliary scanning directions. The other mirror surface core 5 is formed as a single-piece element and is  
25 provided with four mirror surface portions 5a that have concave

sectional shapes in at least the auxiliary scanning direction.

If the mirror surface cores are independent of one another (i.e., one core corresponds to one lens surface), there may be relative positional errors among the respective mirror surface cores. Since the positional error of the cores results in the positional error among the lens surfaces of the molded complex lens, the image forming performance deteriorates.

On the other hand, since the incident lens surfaces 21 and the exit lens surfaces 22 are formed by the single-piece mirror surface cores 4 and 5, respectively, during the molding process, the relative positional error among the incident lens surfaces 21 and the relative positional error among the exit lens surfaces 22 can be reduced. Further, since the mirror surface portions 4a and 5a have concave sectional shapes in the auxiliary scanning direction, each of the boundaries of the mirror surface portions 4a and 5a are formed as a peak that can be sharply processed by the cutting tool. Therefore, the mirror surface portions can be processed without the margins at the boundary portions, which avoids upsizing of the lens surfaces 21 and 22 in the auxiliary scanning direction more than necessary.

Fig. 4 is a general description of a tandem scanning optical system, which employs the complex lens manufactured by the above-described method, in the auxiliary scanning direction.

The tandem scanning optical system deflects the four laser beams, which are emitted from light source portion (not shown) and modulated independently, by means of a polygon mirror 30 at the same time, and converges the four laser beams onto the 5 respective photoconductive drums 41, 42, 43 and 44. Rotation of the polygon mirror 30 about a rotation axis 30a scans the laser beam on the photoconductive drums to form four scanning lines at the same time.

An  $f\theta$  lens to converge the light beams consists of a first 10 lens 51 and a second lens 52 that are located in the vicinity of the polygon mirror 30, and third lenses 53a, 53b, 53c and 53d that are located on the respective optical paths divided by mirrors 71 to 78. The first and second lenses 51 and 52 are the complex lenses, each of which is formed as a single-piece 15 element and it is equivalent to the combination of four independent lens portions stacked one on another as shown in Fig. 1B. Further, each of the lens surfaces of the first and second lens 51 and 52 seems like a flat surface in Fig. 4, while it is not flat surface. Each of the surfaces of the 20 first and second lenses 51 and 52 is a combination surface having four lens portions.

In Fig. 4, the laser beam deflected by the polygon mirror 30 at the highest point among the four laser beams passes through the highest lens portions of the first and second 25 lenses 51 and 52. The laser beam is reflected by the mirror 71

upwards and then reflected by the mirror 72 downwards. The reflected laser beam passes through the third lens 53a and is converged onto the photoconductive drum 41. In the same manner, the second, third and fourth laser beams from the top 5 pass the second, third fourth lens portions of the first and second lenses 51 and 52, and they are reflected by the mirrors 73, 75 and 77 to the upside and then reflected by the mirrors 74, 76 and 78 to the downside, respectively. The reflected second, third and fourth laser beams pass through the third 10 lenses 53b, 53c and 53d and are converged onto the photoconductive drums 42, 43 and 44, respectively.

Next, two embodiments of the tandem scanning optical system whose generic constructions are shown in Fig. 4 will be described. In the following description, the optical system 15 for the first laser beam deflected by the polygon mirror 30 at the highest point is taken out from the four optical systems. Further, the optical path is developed by omitting the mirrors 71 and 72.

20 First Embodiment

Figs. 5 and 6 show a scanning optical system of a first embodiment in the main scanning direction and in the auxiliary scanning direction, respectively. Fig. 5 shows optical elements from a cylindrical lens 31 to the photoconductive drum 41; and Fig. 6 shows optical elements from the polygon mirror 25

30 to the photoconductive drum 41.

The following TABLE 1 shows the numerical construction of the scanning optical system according to the first embodiment.

Symbol  $f$  in the table represents a focal length of the  $f\theta$  lens in the main scanning direction,  $W$  represents the width of the scanning range,  $r_y$  is a radius of curvature (unit: mm) of a surface in the main scanning direction,  $r_z$  denotes a radius of curvature (unit: mm) of a surface in the auxiliary scanning direction (which will be omitted if a surface is a rotationally-symmetrical surface),  $d$  is a distance (unit: mm) between surfaces along the optical axis,  $n$  is a refractive index of an element at a design wavelength 780 nm.

Surface numbers 1 and 2 represent the cylindrical lens 31, a number 3 represents the reflection surface of the polygon mirror 30, numbers 4 and 5 represent the first lens 51 of the  $f\theta$  lens, numbers 6 and 7 represent the second lens 52 of the  $f\theta$  lens, numbers 8 and 9 represent the third lens 53a of the  $f\theta$  lens.

TABLE 1

f = 200.0 mm W = 216 mm

Surface Number	ry	rz	d	n
1	$\infty$	50.00	4.00	1.51072
2	$\infty$	-	97.00	
3	$\infty$	-	33.00	
4	$\infty$	-	10.00	1.48617
5	-199.80	-	4.00	
6	$\infty$	-	10.00	1.48617
7	-170.00	-	93.00	
8	-540.00	30.38	4.00	1.48617
9	-1045.00	-	95.10	

The surface of number 1 is a cylindrical surface having a power only in the auxiliary scanning direction, the surfaces of numbers 2 and 3 are flat surfaces, the surfaces of numbers 4, 5, 6, 7 and 9 are rotationally-symmetrical aspherical surfaces, and the surface of number 8 is an anamorphic aspherical surface.

A rotationally-symmetrical aspherical surface is defined by distribution of sag amount  $X(h)$ . The sag  $X(h)$  is a distance of the point on the aspherical surface whose distance from the optical axis is  $h$  with respect to the tangential plane at the optical axis. The sags  $X(h)$  is expressed by the following equation (1);

$$(1) \quad X(h) = \frac{Ch^2}{1 + \sqrt{1 - (\kappa + 1)^2 C^2 h^2}} + A_4 h^4 + A_6 h^6 + A_8 h^8$$

Symbol  $C$  is a curvature ( $1/r$ ) on the optical axis,  $\kappa$  is a conic constant,  $A_4$ ,  $A_6$  and  $A_8$  are aspherical surface

coefficients of fourth, sixth and eighth orders.

The various constants and coefficients for defining the rotationally-symmetrical surfaces are shown in TABLE 2.

5 TABLE 2

Surface Number	$\kappa$	$A_4$	$A_6$	$A_8$
4	0.00	$3.58 \times 10^{-6}$	$-5.09 \times 10^{-10}$	0.00
5	0.00	$2.84 \times 10^{-6}$	$-1.33 \times 10^{-10}$	$1.00 \times 10^{-14}$
6	0.00	$1.03 \times 10^{-6}$	$1.96 \times 10^{-11}$	0.00
7	0.00	$1.06 \times 10^{-6}$	$3.00 \times 10^{-10}$	0.00
9	0.00	$-4.47 \times 10^{-8}$	$-1.53 \times 10^{-12}$	$-1.49 \times 10^{-16}$

It should be noted that the radii of curvature of the aspherical surfaces indicated in TABLE 1 are values on the optical axis.

10 The anamorphic aspherical surface (surface number 8) is a surface whose radius of curvature in the auxiliary scanning direction is determined by the distance from the optical axis in the main scanning direction and it does not have a rotation axis. The anamorphic aspherical surface is defined by the 15 following two equations (2) and (3).

$$(2) X(Y) = \frac{CY^2}{1 + \sqrt{1 - (\kappa + 1)^2 C^2 Y^2}} + A_4 Y^4 + A_6 Y^6 + A_8 Y^8 + A_{10} Y^{10}$$

$$(3) \frac{1}{rz(Y)} = \frac{1}{rz_0} + B_1 Y + B_2 Y^2 + B_4 Y^4 + B_6 Y^6$$

The shape of the anamorphic aspherical surface in the main scanning direction is defined by the sag  $X(Y)$  according to the

equation (2). The sag  $X(Y)$  is a distance of the point on the aspherical surface whose distance from the optical axis is  $Y$  in the main scanning direction with respect to the tangential plane at the optical axis.

5 A radius of curvature in the auxiliary scanning direction varies in accordance with the distance  $Y$  from the optical axis in the main scanning direction. The radius of curvature  $rz(Y)$  of the surface in the auxiliary scanning direction at the point where the distance from the optical axis is  $Y$  is expressed by  
10 the equation (3).

Symbols in the equation (2) are the same as in the equation (1). The values  $B_1$ ,  $B_2$ ,  $B_4$  and  $B_6$  are coefficients that define the radius of curvature in the auxiliary scanning direction,  $rz_0$  is a radius of curvature in the auxiliary scanning direction on the optical axis (equal to  $rz$  in TABLE  
15 1). The coefficients that define the surface of number 8 are shown in TABLE 3.

TABLE 3

$K$	0.00	$B_1$	$-1.89 \times 10^{-6}$
$A_4$	$1.08 \times 10^{-7}$	$B_2$	$-1.16 \times 10^{-6}$
$A_6$	$-1.08 \times 10^{-11}$	$B_4$	$5.36 \times 10^{-12}$
$A_8$	$3.88 \times 10^{-16}$	$B_6$	$2.52 \times 10^{-15}$
$A_{10}$	0.00	-	-

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Figs. 7A and 7B are graphs showing the optical performance of the scanning optical system of the first embodiment; Fig. 7A

shows a linearity error that is a deviation of the real beam spot with respect to the ideal beam spot in the main scanning direction; and Fig. 7B shows a curvature of field that is a distance from the design image surface to the beam waist. In 5 the graph of Fig. 7B, a dotted line indicates the values in the main scanning direction and a solid line indicates the values in the auxiliary scanning direction.

#### Second Embodiment

10 Figs. 8 and 9 show a scanning optical system of a second embodiment in the main scanning direction and in the auxiliary scanning direction, respectively. The following TABLE 4 shows the numerical construction of the scanning optical system according to the second embodiment. The relationship between 15 the surface numbers and the optical elements are identical to the first embodiment.

TABLE 4

 $f = 200.0 \text{ mm}$   $W = 216 \text{ mm}$ 

Surface Number	Ry	rz	d	n
1	$\infty$	50.00	4.00	1.51072
2	$\infty$	-	97.00	
3	$\infty$	-	46.50	
4	-75.00	1000.00	5.00	1.48617
5	-69.10	-400.70	2.00	
6	$\infty$	-	10.00	1.51072
7	-115.80	$\infty$	106.50	
8	-722.70	29.71	4.00	1.48617
9	-1750.80	-	90.00	

The surface of number 1 is a cylindrical surface having a power only in the auxiliary scanning direction, the surfaces of numbers 2, 3 and 6 are flat surfaces, the surfaces of numbers 4 and 5 are toric aspherical surfaces, the surface of number 7 is a cylindrical surface having a power only in the main scanning direction, the surface of number 8 is an anamorphic aspherical surface and the surface of number 9 is a rotationally-symmetrical aspherical surface.

The toric aspherical surface is defined by the shape in the main scanning direction that is represented by the equation (2) and the radius of curvature in the auxiliary scanning direction rz. The toric aspherical surface is defined as a locus of the aspherical curve line defined by the equation (2) when the aspherical curve line rotates about the axis extending in the main scanning direction that crosses the optical axis at the point whose distance from the surface along the optical

axis equals to  $rz$ .

The various constants and coefficients for defining the toric aspherical surfaces and the rotationally-symmetrical surface are shown in TABLE 5. The various constants and 5 coefficients for defining the anamorphic aspherical surface are shown in TABLE 6.

TABLE 5

Surface Number	$\kappa$	$A_4$	$A_6$	$A_8$
4	0.00	$2.93 \times 10^{-6}$	$2.35 \times 10^{-10}$	0.00
5	0.00	$2.56 \times 10^{-6}$	$3.83 \times 10^{-10}$	0.00
9	0.00	$-3.82 \times 10^{-8}$	$3.35 \times 10^{-12}$	$-3.09 \times 10^{-16}$

10 TABLE 6

$\kappa$	0.00	$B_1$	$-1.18 \times 10^{-6}$
$A_4$	$5.39 \times 10^{-8}$	$B_2$	$-9.25 \times 10^{-7}$
$A_6$	$-3.29 \times 10^{-12}$	$B_4$	$2.30 \times 10^{-11}$
$A_8$	$6.43 \times 10^{-18}$	$B_6$	0.00
$A_{10}$	0.00	-	-

Figs. 10A and 10B are graphs showing the optical performance of the scanning optical system of the second embodiment; Fig. 10A shows the linearity error; and Fig. 10B 15 shows the curvature of field.

When the scanning optical systems of the first and second embodiments are applied to the tandem scanning optical system of Fig. 4, each of the first and second lenses 51 and 52 is

formed as the complex lens having four lens portions, each of which is designed according to the data of the embodiments, stacked in the auxiliary scanning direction, and the third lens 53a designed according to the data of the embodiments is also 5 employed as the other third lenses 53b to 53d.

Further, the complex lens is molded by the injection molding of the resin in the embodiment, while the method of the invention can be applied to another molding method employing the molding dies, such as a method to manufacture a glass 10 molding lens or a hybrid lens having a resin layer on a glass lens.

As described above, since the lens surfaces of the complex lens at the incident side are formed by the single-piece mirror surface core and the lens surfaces at the exit side are formed 15 by the other single-piece mirror surface core, the relative positional error among the lens surfaces at the incident side and that at the exit side can be reduced.

Further, when the mirror surface portions have concave sectional shapes in the auxiliary scanning direction, the 20 boundary portions can be sharply processed by the cutting tool. Therefore, the mirror surface portions can be processed without the margins at the boundary portions, which avoids upsizing of the lens surfaces in the auxiliary scanning direction more than necessary.

The present disclosure relates to subject matter contained in Japanese Patent Application No. 2000-358852 filed on November 27, 2000, which is expressly incorporated herein by reference in its entirety.